

L18

Biot-Savart Law

Const current \rightarrow Const \vec{B}

$$\frac{\partial \vec{J}}{\partial t} = 0$$

$$\frac{\partial \vec{B}}{\partial t} = 0$$

$$\vec{J} = \vec{J}(\vec{r})$$

$$\vec{B} = \vec{B}(\vec{r})$$

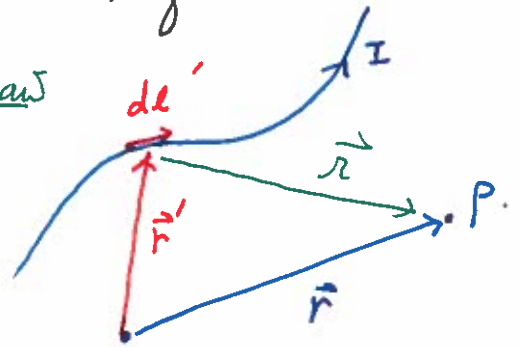
"Steady State $\frac{\partial}{\partial t} = 0$ including $\frac{\partial \rho}{\partial t} = 0$ "

$\therefore \nabla \cdot \vec{J} = 0$ due to continuity Eq. (for steady current)

$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{\vec{I} \times \hat{r}}{r^2} dl'$$

$$= \frac{\mu_0 I}{4\pi} \int \frac{d\vec{l}' \times \hat{r}}{r^2}$$

Biot-Savart law



μ_0 : vacuum permeability
 $\mu_0 = 4\pi \times 10^{-7} \text{ N/A}^2$

$$[B] = [\mu_0][I][\frac{1}{L}] = \frac{N}{A^2} \cdot A \cdot (\frac{1}{m}) = \frac{N}{A \cdot m} = T$$

$$\vec{B} = \frac{\mu_0 I}{4\pi} \int \frac{d\vec{l}' \times \hat{r}}{r^2}$$

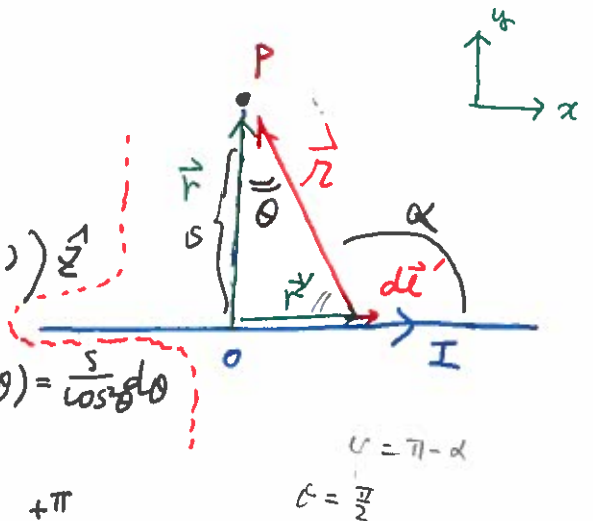
$$d\vec{l}' \times \hat{r} = dl' \sin \alpha = dl' \sin(\frac{\pi}{2} - (\pi - \theta)) \hat{z}$$
$$= dl' \cos \theta \hat{z}$$

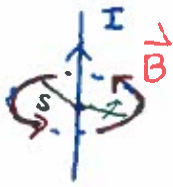
Since $\tan \theta = \frac{r'}{s} \Rightarrow dr' = d(s \tan \theta) = \frac{s}{\cos^2 \theta} d\theta$

where $r = \sqrt{r'^2 + s^2} = \frac{s}{\cos \theta}$

$$\therefore \vec{B} = \frac{\mu_0 I}{4\pi} \int_{-\pi/2}^{+\pi/2} \frac{dr' \cos \theta}{(\frac{s}{\cos \theta})^2} \hat{z}$$

$$= \frac{\mu_0 I}{4\pi} \int_{-\pi/2}^{+\pi/2} \frac{1}{s} \cos \theta d\theta \hat{z} = \frac{\mu_0 I}{2\pi s} \hat{z}$$





$$\vec{B} = \frac{\mu_0 I}{2\pi r} \hat{\phi}$$

L2

Consider two parallel wires carrying current $\vec{I}_1 = I_1 \hat{y}$ & $\vec{I}_2 = I_2 \hat{y}$ ($I_1, I_2 > 0$). At the position of wire 2, the magnetic field from I_1 , \vec{B}_1 , will interact with \vec{I}_2 and exert force.

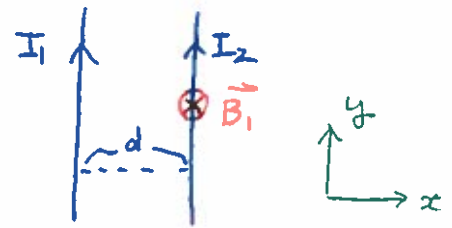
$$\vec{B}_1(d) = -\frac{\mu_0 I_1}{2\pi d} \hat{z}$$

$$\therefore \vec{F}_2 = I_2 \int (d\vec{l}_2 \times \vec{B}_1)$$

$$= -I_2 \frac{\mu_0 I_1}{2\pi d} \int dl_2 (\hat{y} \times \hat{z})$$

$$= -I_2 \frac{\mu_0 I_1}{2\pi d} \int dl_2 (\hat{x}) \quad \text{: attractive force}$$

length of wire.



$$\therefore \vec{f}_2 = \vec{F}_2 / \int dl_2 = -\frac{\mu_0 I_1 I_2}{2\pi d} \hat{x} \quad \text{: force per unit length}$$

$$\vec{I}_1 \cdot \vec{I}_2 > 0 \Rightarrow \text{attractive force}$$

$$\vec{I}_1 \cdot \vec{I}_2 < 0 \Rightarrow \text{repulsive force.}$$

EX

$$\vec{r} = z \hat{z}; \quad \vec{r}' = R \cos \varphi \hat{x} + R \sin \varphi \hat{y}$$

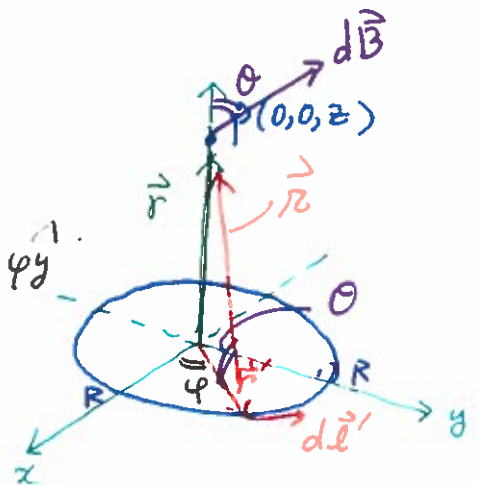
$$\vec{r} = \vec{r} - \vec{r}' = z \hat{z} - R \cos \varphi \hat{x} - R \sin \varphi \hat{y}$$

$$d\vec{l}' = R d\varphi \hat{\phi} = R d\varphi (-\sin \varphi \hat{x} + \cos \varphi \hat{y})$$

$$\therefore d\vec{l}' \times \vec{r} = \frac{1}{R} d\vec{l}' \times \vec{r}$$

$$= \frac{1}{R} R d\varphi (-\sin \varphi \hat{x} + \cos \varphi \hat{y}) \times (z \hat{z} - R \cos \varphi \hat{x} - R \sin \varphi \hat{y})$$

$$= \frac{1}{R} R d\varphi \left\{ R(\sin^2 \varphi + \cos^2 \varphi) \hat{z} + z \cos \varphi \hat{x} + z \sin \varphi \hat{y} \right\}$$



$$\begin{aligned} \therefore \vec{B}(\vec{r}) &= \frac{\mu_0 I}{4\pi} \int \frac{d\vec{l} \times \vec{r}}{r^3} \quad \text{where } r^3 = (z^2 + R^2)^{3/2} = \text{const.} \quad \boxed{3} \\ &= \frac{\mu_0 I}{4\pi} \frac{1}{(z^2 + d^2)^{3/2}} \int_0^{2\pi} d\varphi \left\{ R^2 \hat{z} + Rz \sin\varphi \hat{y} + Rz \cos\varphi \hat{x} \right\} \\ &= \frac{\mu_0 I}{z} \frac{R^2}{(z^2 + d^2)^{3/2}} \hat{z} \end{aligned}$$

Or, by symmetry you know only z-comp. survives.

$$\begin{aligned} \therefore B(z) &= \frac{\mu_0 I}{4\pi} \int \frac{dl' \cos\theta}{r^2} \quad \text{where } \cos\theta = \frac{R}{r} \\ &= \frac{\mu_0 I}{4\pi} \frac{R}{R^3} \int_0^{2\pi} R d\varphi = \frac{\mu_0 I}{4\pi} \frac{2\pi R^3}{R^3} \Rightarrow \text{same result.} \end{aligned}$$

HW 5.9, 5.11, 5.12.

► Divergence and Curl of \vec{B} .

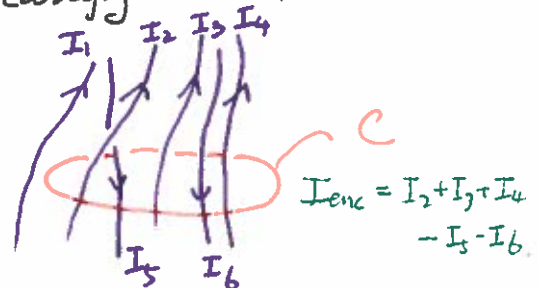
6 Ampere's Law

$$\oint_C \vec{B} \cdot d\vec{l} = \mu_0 \underline{I_{enc}}$$

total current enclosed by C

$$I_{enc} = \int \vec{J} \cdot d\vec{a} \quad \text{for continuous } \vec{J}$$

$$= \sum_{i=1}^n I_i \quad \text{for current carrying wires.}$$



In general, $\oint \vec{B} \cdot d\vec{l} = \int \vec{J} \cdot d\vec{a}$
Stokes' thm

$$\int (\nabla \times \vec{B}) \cdot d\vec{a} = \int \vec{J} \cdot d\vec{a}$$

$\boxed{\nabla \times \vec{B} = \mu_0 \vec{J}}$ Ampere's law in differential form.
~ Gauss's law

6 $\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{I d\vec{l}' \times \hat{r}}{r^2} = \frac{\mu_0}{4\pi} \int \frac{\vec{J}(\vec{r}') \times \hat{r}}{r^2} d\tau'$ ($\vec{r} = \vec{r} - \vec{r}'$)

$$\nabla \cdot \vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \nabla \cdot \left(\frac{\vec{J}(\vec{r}') \times \hat{r}}{r^2} \right) d\tau'$$

$$\nabla \cdot \left(\vec{J} \times \frac{\hat{r}}{r^2} \right) = \frac{\hat{r}}{r^2} \cdot (\nabla \times \vec{J}) - \vec{J} \cdot \left(\nabla \times \frac{\hat{r}}{r^2} \right)$$

$\nabla \cdot (\vec{A} \times \vec{B}) = \vec{B} \cdot (\nabla \times \vec{A}) - \vec{A} \cdot (\nabla \times \vec{B})$

$\therefore \boxed{\nabla \cdot \vec{B} = 0}$

EX \vec{B} from a straight wire carrying I .

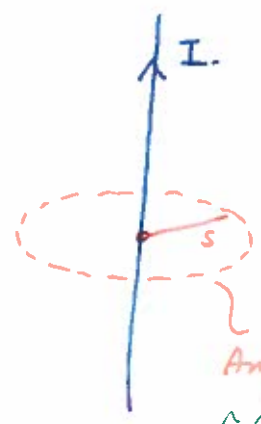
\downarrow
 Cylindrical Sym

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{en}$$

$$2\pi s B = \mu_0 I$$

$$\therefore \vec{B}(s) = \frac{\mu_0 I}{2\pi s} \hat{\phi}$$

on the loop. $|\vec{B}| = B = \text{const}$



Amperian loop
 ~ Gaussian surface

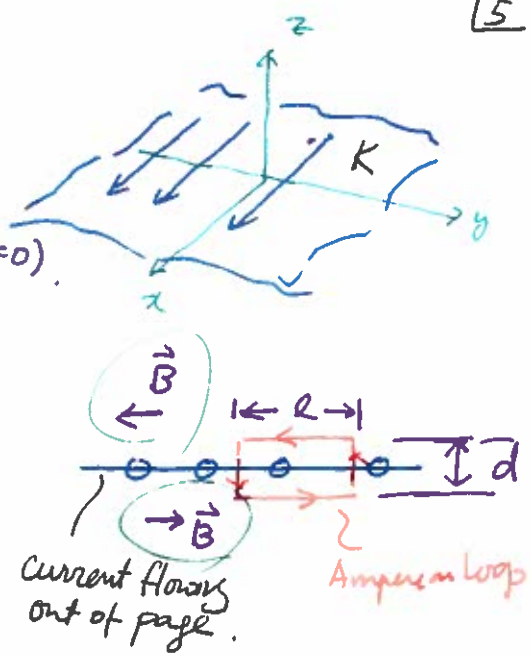
EX

$$\oint_C \vec{B} \cdot d\vec{l} = \mu_0 I_{en}$$

No contribution from the vertical part of the loop ($\because d\vec{l} \cdot \vec{B} = 0$)

$$2Bl = \mu_0 K l$$

$$\therefore \vec{B} = \begin{cases} -\frac{\mu_0 K}{2} \hat{y} & (z > 0) \\ +\frac{\mu_0 K}{2} \hat{y} & (z < 0) \end{cases}$$



EX Solenoid.

For an infinitely long tightly wound solenoid.

$$\vec{B} \sim \hat{z}$$

n : winding # density

Consider the loop (ii) first. for $L \gg 1$.

$$\oint_{(ii)} \vec{B} \cdot d\vec{l} = [-B(a) + B(a+L)] l = 0 \quad \uparrow \text{no current.}$$

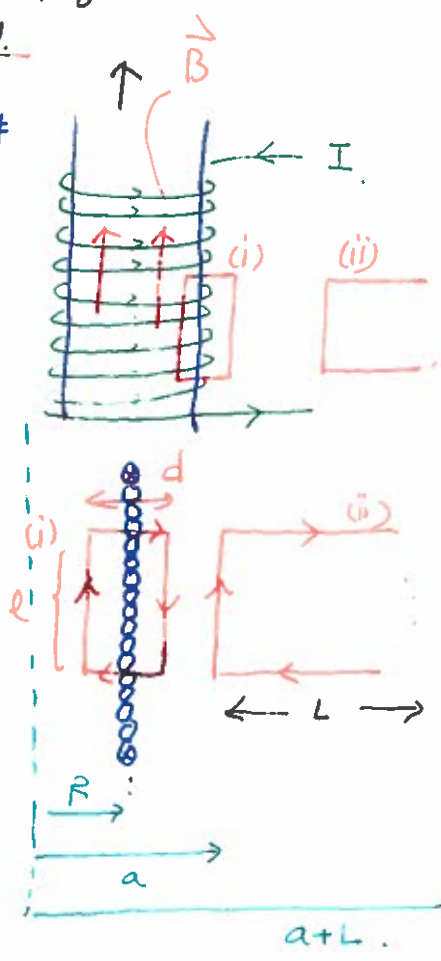
But when $L \rightarrow \infty$, $B \rightarrow 0$

$\therefore B(a) = 0$ (no field outside of solenoid)

Now for loop (i).

$$\oint_{(i)} \vec{B} \cdot d\vec{l} = B_{in} \cdot l - \cancel{B_{out} \cdot l} = \mu_0 n I l$$

$$\therefore \vec{B}_{in} = \mu_0 n I \hat{z}$$



We can position the inside part of the loop anywhere.

Therefore $\vec{B}_{in} = \mu_0 n I \hat{z}$ anywhere inside the infinitely long sol.

HW 5.14, 5.15, 5.17

5.14

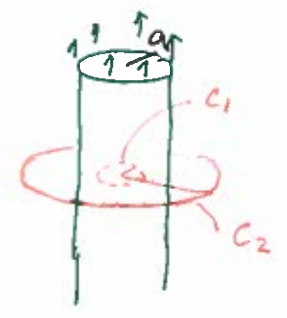
(a) Cylindrical wire of I and radius a

$B(r < a)$

$$\oint_{C_1} \vec{B} \cdot d\vec{\ell} = \mu_0 I_{en} = 0 \quad \therefore B(r < a) = 0$$

For $r > a$

$$\oint_{C_2} \vec{B} \cdot d\vec{\ell} = 2\pi r B_\phi = \mu_0 I \quad \therefore B_\phi = \frac{\mu_0 I}{2\pi r}$$



(b) Solid cylindrical wire of uniform current density, of radius r

$$I = \int \vec{J} \cdot d\vec{a}$$

For $r < a$

$$\oint_{C_1} \vec{B} \cdot d\vec{\ell} = \mu_0 I_{en} = \mu_0 \int \vec{J} \cdot d\vec{a}$$

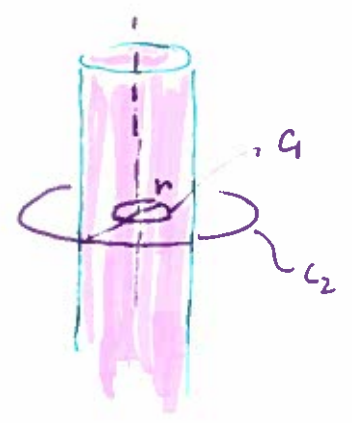
$$2\pi r B_\phi = \mu_0 J (\pi r^2)$$

$$\therefore B_\phi = \frac{\mu_0 J r}{2}$$

For $r > a$

$$2\pi r B_\phi = \mu_0 J (\pi a^2)$$

$$\therefore B_\phi = \frac{\mu_0 J a^2}{2r}$$



(c) For $J = kr$

For $r < a$

$$\oint_{C_1} \vec{B} \cdot d\vec{\ell} = \mu_0 I_{en} = \mu_0 \int_0^r (kr') (2\pi r') dr' = \mu_0 \pi k r^3 \left(\frac{2}{3}\right)$$

$$\therefore B_\phi = \frac{\mu_0 k r^3 \left(\frac{2}{3}\right)}{2r} = \frac{\mu_0 k r^2}{3}$$

For $r > a$

$$I_{en} = \pi k a^3 \left(\frac{2}{3}\right)$$

$$\therefore B_y = \mu_0 \frac{k a^3}{2r} \left(\frac{2}{3}\right) = \mu_0 \frac{k a^3}{3r}$$