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Air resistance (drag)

- drag $F(v)$ depends on the object velocity v
we will consider that $F(v) = -f(v)\hat{v}$

Examples when it is not true.

- airplane, spinning ball, sail boat, ...
- consider case when $v \ll S$ (speed of sound)

$f(v) = bv + cv^2$ - Taylor expansion over v/s

$f_{lin} = bv$ - linear (viscous) drag $\approx \beta Dv$

$f_{quad} = cv^2$ - quadratic drag $\approx \gamma D^2 v^2$

For spherical projectile:
in STP air $\beta = 6.6 \cdot 10^{-4} \text{ NS/m}^2$
 $\gamma = 0.25 \text{ NS}^2/\text{m}^4$

- Reynolds number: $R = Dv \frac{\rho}{\eta}$
 R is a rough approximation for $\frac{f_{quad}}{f_{lin}} = \frac{\gamma}{\beta} Dv$

- Example 2.1

Baseball ($D = 7 \text{ cm}$, $v \sim 5 \text{ m/s}$) $\frac{f_q}{f_l} \sim 570$

Millikan oil drop ($D \approx 1.5 \mu\text{m}$, $v \sim 10^{-4} \text{ m/s}$) $\frac{f_q}{f_l} \sim 10^{-7}$

f_q is dominant when R is large
 f_l is dominant when R is small

- Linear air resistance

$m\dot{\vec{v}} = m\vec{g} - b\vec{v}$

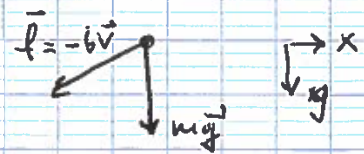
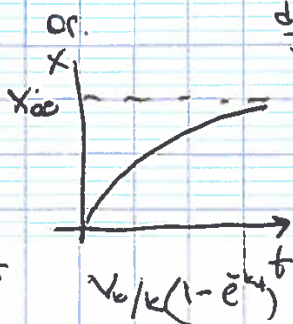
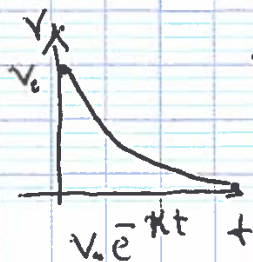
$m\dot{v}_x = -bv_x$
 $m\dot{v}_y = mg - bv_y$ } independent equations for x & y components.

- solution for x:

$\dot{v}_x = -\frac{b}{m}v_x = -kv_x$

or $\frac{dv_x}{v_x} = -k dt \rightarrow \int \frac{dv_x}{v_x} = \int -k dt$

$v_x = v_0 e^{-kt}$ $\leftarrow \ln \frac{v_x}{v_0} = -kt$



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Solution for y: case a) $\uparrow v_y = v_0$ $\downarrow g$
 $\dot{v}_y = g - \frac{b}{m} v_y$ case b) $\downarrow v_y = v_0$ $\downarrow g$
 regardless how the motion starts (initial cond)
 the projectile will be falling down and
 reach its terminal velocity $v_t = \frac{mg}{b}$.

* v_t for small drops

$b = \beta D$ $m = \rho \pi D^3 / 6$

$v_t = \frac{\rho \pi D^2}{6 \beta} g$

$\beta = 1.6 \cdot 10^{-4}$

$v_{ter} = \frac{840 \pi (1.5 \cdot 10^{-6})^2 \cdot 9.8}{6 (1.4 \cdot 10^{-4})} \approx 6 \cdot 10^{-5} \text{ m/s}$

case b)

$\dot{v}_y = \frac{b}{m} (v_t - v_y) = -\frac{b}{m} (v_y - v_t)$

$u = v_y - v_t$ $\frac{du}{dt} = \frac{dv_y}{dt} = \dot{v}_y = \dot{u} \rightarrow \dot{u} = -\frac{b}{m} u$

same equation as for x case: $u = A e^{-kt}$

$v_y - v_t = (v_{y0} - v_t) e^{-kt}$ defined A from initial conditions

$v_y(t) = v_{y0} e^{-kt} + v_t (1 - e^{-kt})$

$v_y(\infty) = v_t$

* characteristic time $v_t = g/k = g\tau$

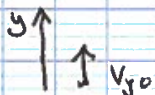
$v_{y0} = 0 \rightarrow v_y(t) = v_t (1 - e^{-t/\tau})$

in $t = \tau$ a falling object reaches 63% of v_t

or τ is time when object reaches v_t if accelerated with const $a = g$.

case 2)

Case a)



reverse y axis $\rightarrow v_t \rightarrow -v_t$

$v_y(t) = v_{y0} e^{-t/\tau} - v_t (1 - e^{-t/\tau})$

$v_y(0) = v_{y0}$

$v_y(\infty) = -v_t$

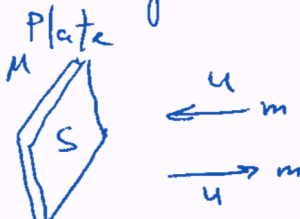
$y(t) = \int_0^t v_y dt = -v_t t + (v_{y0} + v_t) \tau (1 - e^{-t/\tau})$

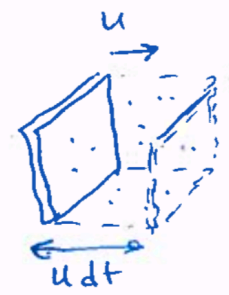
projectile reaches max elevation

$y_{max} = y(t_m)$ when $v_y(t_m) = 0$

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Origin of the quadratic drag

a)  $M \gg m$
 $\Delta P = 2um$ - momentum transfer from particle m to the plate.
 Δt - interaction time.
 $\frac{\Delta P}{\Delta t} = F$ force on the plate

b)  plate moving in ideal gas
 n - number of particles per unit of volume
 u - velocity of the plate
 S = area of the plate.

$\Delta P = mu$ - momentum transfer from a single particle.
 $nuSdt$ - number of interacting particles in time Δt .

$$\frac{\Delta P}{\Delta t} = \frac{\Delta P}{\Delta t} \cdot nuS \cdot dt = mnSu^2$$

Drag Coefficient Values
 Typical values of drag coefficient C .

Object	C
Airfoil	0.05
Toyota Camry	0.28
Ford Focus	0.32
Honda Civic	0.36
Ferrari Testarossa	0.37
Dodge Ram pickup	0.43
Sphere	0.45
Hummer H2 SUV	0.64
Skydiver (feet first)	0.70
Bicycle	0.90
Skydiver (horizontal)	1.0
Circular flat plate	1.12

Quadratic drag force
 for objects of different shape

$$F_{quad} = \frac{1}{2} C \rho S u^2$$